A Fundamental Study on the High-power Fiber Laser Cleaning for Removing the Multi-layer Coating

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Abstract

The mechanical cleaning technology used in existing coating removal processes, such as blasting and grinding, has various problems, including environmental pollution owing to fine dust, worker welfare problems, and increased process time. As an alternative, an eco-friendly laser cleaning technology has attracted attention. However, research on high-power laser cleaning technology for removing thick coating layers and repairing large areas is limited. In this study, a high-power fiber laser with an average power of 1 kW was used to conduct cleaning experiments to remove a multi-layer coating with a thickness of approximately 340 μm; this coating is applied to improve the corrosion resistance of steel used for shipbuilding. As a result of experiments based on the main process parameters, such as energy density, average power, and beam mode, the cleaning performance can be significantly improved under a high power density. Moreover, because it exhibits a large difference in surface roughness controllability for each beam mode, it is estimated that the utilization of laser cleaning technology can be maximized depending on the application part.

Key Words : High-power laser cleaning process, Eco-friendly technology, Multi-layer coating

1. Introduction

A multi-layer coating is a coating system that allows steel structures placed in severe corrosive environments such as marine structures, power plants, and ships to withstand extended exposure to such corrosive conditions. In particular, multi-layer coatings used in the shipbuilding industry consist of multiple layers since a single layer coating is unable to provide excellent adhesive properties, corrosion resistance, and aesthetics.

Over time, these multi-layer coatings also need to be removed and recoated if they reach the end of their service life or accumulate damage such scratches. Mechanical cleaning technologies such as blasting and grinding have been applied to current coating removal processes, but these techniques suffer from serious environmental pollution, present risks to the health and safety of workers, and face problems of increased lead time due to the hazardous processing environment. To overcome these challenges, there is a growing need for the development of laser cleaning technology employing an environmentally friendly laser heat source for the removal of coating layers.

Existing studies on coating layer removal primarily consist of research on the removal of a single layer of epoxy paint and primer according to process parameters using a low-power laser with an average power less than 500 W. Moreover, Marimuthu et al. extended the use of laser cleaning for paint removal to the removal of various contaminants such as TiN coating, oil, and grease on the surface of a material. However, when a low-power laser is used to remove coating layers of thick films that have a thickness of hundreds of micrometers similar to multi-layer coatings as well as oxide layers that have a high boiling point and are more...
tightly bound than coating layers, the cleaning time may significantly increase and complete removal may be difficult. Therefore, it is necessary to develop a cleaning technology employing a high-power laser with an average power above 500 W. Shamsujjoha et al. used a Nd:YAG laser with an average power above 1 kW to remove paint with a thickness of approximately 200 μm and subsequently characterized the mechanical properties and morphology of the cleaned surface, but discussion on the dominant processing parameters during laser cleaning is lacking. Shamsujjoha et al. investigated the effect of average power and energy density during laser cleaning by using a high-power diode laser with an average power of 2.5 kW to remove a 350 μm-thick coating layer composed of 5 layers. However, analysis on changes in the surface and cross-section of the cleaned area with respect to processing parameters was not performed.

As described above, high-power laser cleaning is known to be highly advantageous for the removal of coating layers of thick films, but there is still a substantial lack of research on this technology. Therefore, in this work, high-power fiber laser cleaning at an average power of 1 kW was employed for the removal of multi-layer coatings in shipbuilding, and the effect of laser cleaning according to energy density and beam mode at each power setting was investigated from various aspects.

2. Experimental materials and methods

The material used in experiments is a multi-layer coated steel, and the cross-sectional image of the test specimen is presented in Fig. 1. The coating system consists of 4 different layers. The first layer is a shop primer with a thickness of approximately 10 μm. The second and third layers are coated with epoxy paint, and the thickness of each layer is approximately 130 μm and 100 μm, respectively. A red anti-fouling paint is applied at the top layer, and the thickness of the coating layer is approximately 100 μm, resulting in an overall coating layer thickness of 340 μm.

Fig. 2 shows the laser cleaning equipment used in experiments, which employs a Q-switching fiber laser with an average power of 1 kW. Specifications of the laser cleaning equipment are presented in Table 1. The optical system for cleaning consists of a 1.2×1.2 mm square beam with a multi-mode beam mode, 2D scanner, and scan lens. The laser beam irradiated onto the test specimen was fixed at a pulse overlap rate \( R_{po} \) of 50 % and line overlap rate \( R_{lo} \) of 20 %. Detailed experimental conditions are listed in Table 2. Experiments were conducted by varying the energy density \( D_{e} \), which is the main parameter during laser cleaning.

![Fig. 1 Cross-section of the specimen](image)

![Fig. 2 Setup of experimental equipment for laser cleaning](image)

<table>
<thead>
<tr>
<th>Parameter</th>
<th>( D_{e} (\text{J/cm}^2) )</th>
<th>( f_0 (\text{kHz}) )</th>
<th>( E_{p} (\text{mJ}) )</th>
<th>( P_{ave} (\text{W}) )</th>
<th>( v (\text{m/s}) )</th>
<th>( R_{po} (%) )</th>
<th>( R_{lo} (%) )</th>
<th>( \tau_p (\text{ns}) )</th>
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<td>5.9</td>
<td>17</td>
<td>58.8</td>
<td>1000</td>
<td>8.5</td>
<td>50</td>
<td>20</td>
<td>100</td>
<td></td>
</tr>
<tr>
<td>7.1</td>
<td>15</td>
<td>71.4</td>
<td></td>
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<td></td>
<td></td>
<td></td>
<td></td>
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<tr>
<td>8.3</td>
<td>12</td>
<td>83.3</td>
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</table>

Table 1 Specification of laser cleaning equipment

Table 2 Experimental conditions with energy density

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3. Results and discussion

3.1 Effect of energy density

The effect of energy density during laser cleaning was investigated by changing the energy density to 5.9 J/cm², 7.1 J/cm², and 8.3 J/cm². Representative images of the surface and cross-section of the laser-cleaned area based on the number of scans at an energy density of 5.9 J/cm² are shown in Fig. 3. The red anti-fouling paint at the topmost layer can be observed in the sample before laser cleaning, while the anti-fouling paint is removed after 25 scans and the third layer is exposed. The third layer is removed after 35 scans, and the second layer remains; increasing the number of scans to 45 demonstrates that all coating layers on the surface of the base metal are removed.

X-ray diffraction (XRD) analysis was conducted to examine the change in composition of the laser-cleaned surface according to the number of scans, and the results are shown in Fig. 4. The number of scans was varied from 25 to 45 at intervals of 5, and the change in composition of each layer was clearly distinguishable. Components of the anti-fouling paint were detected in the uncleaned test specimen, while those of epoxy paint were detected after 25–35 scans. In addition, some of the base metal was exposed as more paint layers were removed, resulting in the detection of Fe, the element of the base metal. When the number of scans was increased above 40, all components of the paint were removed and only the elements of the base metal were detected. However, comparing the XRD results and surface images suggested that complete removal of all coating layers was achieved at 45 scans.

Fig. 5 shows the change in residual coating thickness with respect to increasing number of scans at each energy density. It can be seen that the thickness gradually decreases with increasing number of scans as the coating layers become vaporized by the laser heat source, and complete removal is achieved with 45 scans at an energy density of 5.9 J/cm², 40 scans at 7.1 J/cm², and 35 scans at 8.3 J/cm². As the energy density increases, the amount of laser energy irradiated on the material increases, making it easier to raise the temperature of the surface to the boiling point of the paint. Thus, at a higher energy density, the relative amount of material that is evaporated and removed upon each laser scan increases, such that removal of the coating layers can be achieved with relatively fewer scans.

![Fig. 3](link) Surface and cross-section of the laser cleaned surface with the number of scans in De : 5.9 J/cm²

![Fig. 4](link) XRD results of the laser cleaned surface in De : 5.9 J/cm²

![Fig. 5](link) Residual coating thickness distribution with the number of scans and energy density
3.2 Effect of average power and beam mode

Lasers with an average power of 1 kW and 200 W were used in laser cleaning experiments that investigated the effect of average power, and the detailed test conditions are listed in Table 3. In these experiments, the beam modes of the 1 kW laser and 200 W laser were respectively set to multi mode and single mode, and the schematic of the beam profile of each laser is shown in Fig. 6. The multi mode laser exhibits a top-hat profile with a large spot diameter and uniform distribution of power density across the entire beam, while the single mode laser shows a Gaussian profile with a small spot diameter and maximum power density at the center of the beam. As such, lasers with different average power and beam mode were used to compare and analyze the cleaning effect.

Fig. 7 displays the images of the surface and cross-section of the laser cleaned area at each average power and number of scans. Coatings on the base metal were fully removed after 40 scans using the 1 kW laser and 16 scans using the 200 W laser. The reduction in cleaning effect in the former case despite the use of a laser with a higher average power is attributed to the difference in power density. Calculations on the power density \(D_p\) affecting the removal process of each laser show that the 1 kW and 200 W lasers have a power density of \(57.8 \times 10^6\) and \(129.8 \times 10^6\), respectively. Hence, the performance of coating layer removal can be enhanced by using the single mode laser with a highly concentrated energy owing to the high intensity of the laser heat source penetrating into the material. In contrast, using the multi mode laser beam with a top-hat distribution resulted in an increase in the number of scans for coating layer removal due to its relatively lower power density.

3.3 Comparison of surface characteristics

The processing parameters of laser cleaning also have a significant effect on the surface characteristics of the cleaned area. In this section, the effect of pulse duration time \(\tau_p\) and beam mode was analyzed. The laser pulse width refers to the time over which the beam irradiates from the pulse laser. As shown in the images of the laser cleaned surface at each average power (Fig. 7), using the 1 kW laser led to a discoloration that was caused by thermal diffusion from a relatively longer laser irradiation time resulting in thermal effects on the base metal underneath the coating layers.

In addition, the surface roughness profile of the cleaned surface at different beam modes is shown in Fig. 8. As shown in Fig. 8(a), owing to the consistent energy distribution and relatively large beam size, the laser beam with a top-hat profile leads to a smooth surface more

![Fig. 6 Power density distribution of the gaussian and top-hat profile](image)

Table 3 Laser radiation conditions with average power

<table>
<thead>
<tr>
<th>Parameter (P_{\text{ave}}(W))</th>
<th>Beam mode</th>
<th>(D_p(W/cm^2))</th>
<th>(D_e(\mu m))</th>
<th>(E_p(mJ))</th>
<th>(f_p(kHz))</th>
<th>(v(m/s))</th>
<th>(R_{\text{po}}(%))</th>
<th>(R_{\text{lo}}(%))</th>
<th>(\tau_p(ns))</th>
<th>(\text{Focal spot diameter})</th>
</tr>
</thead>
<tbody>
<tr>
<td>1,000 Multi mode</td>
<td></td>
<td>57.8 (\times 10^6)</td>
<td>8.3</td>
<td>83.3</td>
<td>12</td>
<td>6</td>
<td>50</td>
<td>20</td>
<td>100</td>
<td>1.2 (\times 1.2) mm</td>
</tr>
<tr>
<td>200 Single mode</td>
<td></td>
<td>129.8 (\times 10^6)</td>
<td>7.8</td>
<td>1</td>
<td>200</td>
<td>10</td>
<td>60</td>
<td>20</td>
<td>60</td>
<td>128 (\mu m)</td>
</tr>
</tbody>
</table>

\*\(E_p\) : pulse energy, \(f_p\) : pulse frequency, \(v\) : scan speed

![Fig. 7 Surface and cross-section of the laser cleaned surface with the average power](image)
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1) Cleaning experiments under different energy density settings revealed that complete removal of multi-layer coatings was achieved with relatively smaller number of scans at a higher energy density, since the amount of laser energy irradiating on the material increased and made it easier to raise the temperature of the surface to the boiling point of the paint.

2) Analysis on the effect of average power and beam mode during laser cleaning demonstrated that a single mode laser with an average power of 200 W and a high power density has a strong intensity for deep penetration into the material and showed superior cleaning performance to that of the multi mode laser.

3) In addition, it was confirmed that the pulse width of a laser has a significant effect on the heat input into the material and that the laser beam mode can minimize damage to the base metal or create an artificial surface roughness.

4) Based on these research results on laser cleaning, it is believed that eco-friendly laser cleaning technology will show increased applicability in the shipbuilding and marine industry.

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